

Model Calculations of Non-Symmetric SLS Sextupole

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Model Calculations

These calculations are based on the information available

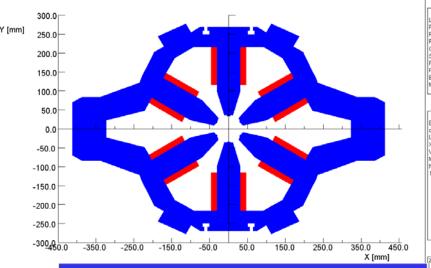
Expect differences between the calculations and measurements from

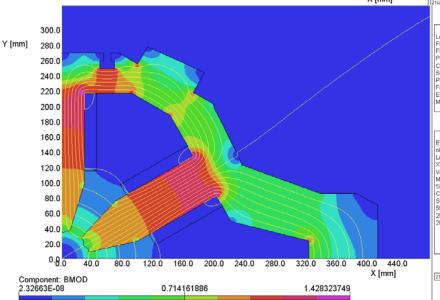
- Differences between the drawings available and the drawings/sketches based on which the laminations for magnet were cut by the vendor
- Actual laminations Vs. drawings (i.e. inspection report on laminations, etc.)
- Shimming, chamfering and other corrections in a particular magnet
 - We are told it was done after measurements a right thing to do, and that's what we would do, but it could cause a large difference between calculation and measurements
- Inherent errors in measurements and calculations (2-d calculations are generally more accurate because of number of mesh points and complexities, but if the magnet is short 3-d would be more representative)



Allowed and Non-allowed Harmonics

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PROBLEM DATA
E-loperalls 2/swiss/sex.tup
olesis-asym-80d-full.op2
inear elements
(7 symmetry
//ector potential
Magnetic fields
No mesh
112 regions



PROBLEM DATA
E toperaits Zisowissis exctup
oleksis-asym-90d st
Linear elements
XY symmetry
Vector potential
Magnetic fields
Static solution
Case 15 of 18
Scale factor = 1,5
59433 elements
29989 nodes
28 regions

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Vector Fields

This sextupole does not have the ideal 12-fold symmetry/asymmetry

The coil still has the right symmetry (except for the small end effects); but the iron has only 4-fold symmetry (dipole type rather than sextupole type).

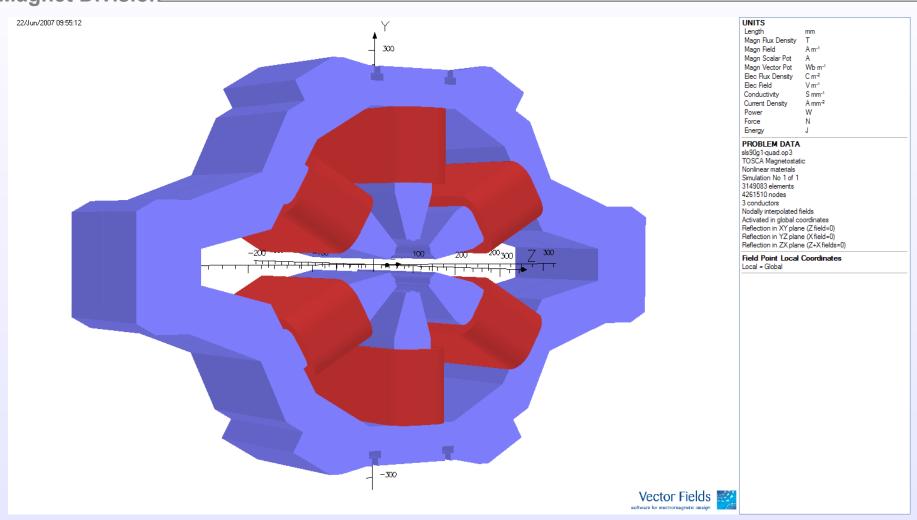
Therefore, in addition to b9, b15, b21, also expect b1, b3, b7, b11,...

All other harmonics (e.g. all skew terms) are either due to construction errors or measurement errors



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3-d Model



Several variants of this model were made to study the influence of chamfering (end)



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BNL Measurements (integral) at 25 mm ~100 A, up ramp

n	an	bn			
1	-11.21	-35.88			
2	-1.36	-1.64			
3	-0.10	10000			
4	-1.01	-0.65			
5	0.97	-4.63			
6	-0.48	0.45			
7	-0.57	0.99			
8	-0.09	0.05			
9	0.14	-2.01			
10	0.01	0.14			
11	-0.02	0.15			
12	-0.09	0.10			
13	-0.12	-0.04			
14 ,	-0.18	-0.18			

In addition to b9, b15, b21, also expect b1, b3, b7, b11,... due to broken symmetry.

All other harmonics (e.g. all skew terms) are either due to construction errors or measurement errors.

This sextupole does not have the ideal 12-fold symmetry/asymmetry

The coil still has the right symmetry (except for the small end effects);

but the iron has only 4-fold symmetry (dipole type rather than sextupole type).



3-d Model Results at 100 A

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Symmetry (and some lack of it) will allow the following normal harmonics:

	n	1	5	7	<mark>/</mark>	11	13	7	17	19	<mark>/</mark>	23	2
No chamfe	er	-109.12	-17.55	4.90	! <mark>/</mark>	1.40	-0.54		0.08	-0.09		-0.07	0.0
Chamfer 1	10	-103.89	-16.27	4.36		1.15	-0.43		0.15	-0.07		-0.07	0.0
Chamfer A	4	-107.93	-17.01	4.58		1.32	-0.51		0.08	-0.09		-0.07	0.0
Chamfer [)25	-103.94	-16.81	4.80		1.37	-0.71		0.23	0.01		-0.04	0.0
Chamfer b	est guess	-106.50	-16.91	4.63		1.28	-0.48		0.12	-0.08		-0.07	0.0
2-d harmo	nics	-57.02	-13.44	6.09		1.76	-0.54		0.21	0.03		-0.08	0.0
Measured		-35.88	-4.50	1.00		0.21	-0.06						
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Given all the uncertainties, the measurements and calculations are closer than what I would have expected.

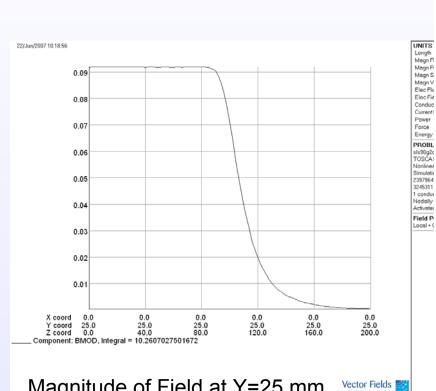
3-d model do not include leads and any other 3-d material

- •For allowed terms (b9, b15, b21, etc.), 3-d models are more reliable in short magnets because of importance of end geometry.
- •For semi-allowed terms (b1, b5, b7, b11, b13, b17, etc., 2-d models are more reliable because of better meshing, etc.

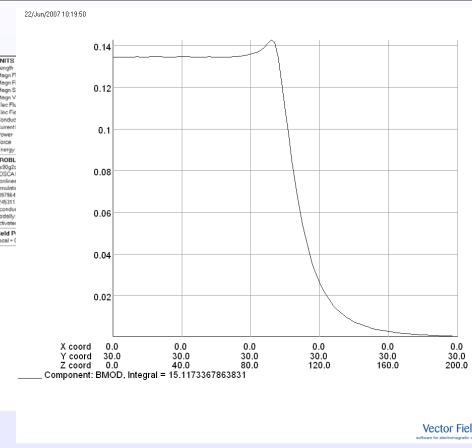


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Field Profile







Magnitude of Field at Y=30 mm (Influence of end can be seen) Variation in chamfering showed significant variation in field